



Mitigation Enabling Energy Transition in the MEDiterranean region

**EN Testing standards for Air conditioners, heat pumps and
liquid chilling packages
Space cooling/heating and domestic hot water applications**

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Contents

- EN 14511:2022 parts 1 to 4
 - Basic test methods
- EN 14825:2022
 - Testing at part load and calculations for SEER and SCOP
- EN 12102-1:2022
 - Sound power testing for AC/HP/LCP
- EN 16147:2017
 - DHW application testing for COP (among others)
- EN 12102-2:2019
 - Sound power testing for DHW production heat pumps

EN 14511:2022 Series

Air conditioners, liquid chilling packages and heat pumps with electrically driven compressors for space heating and cooling.

Part 1: Terms and definitions

Part 2: Test conditions

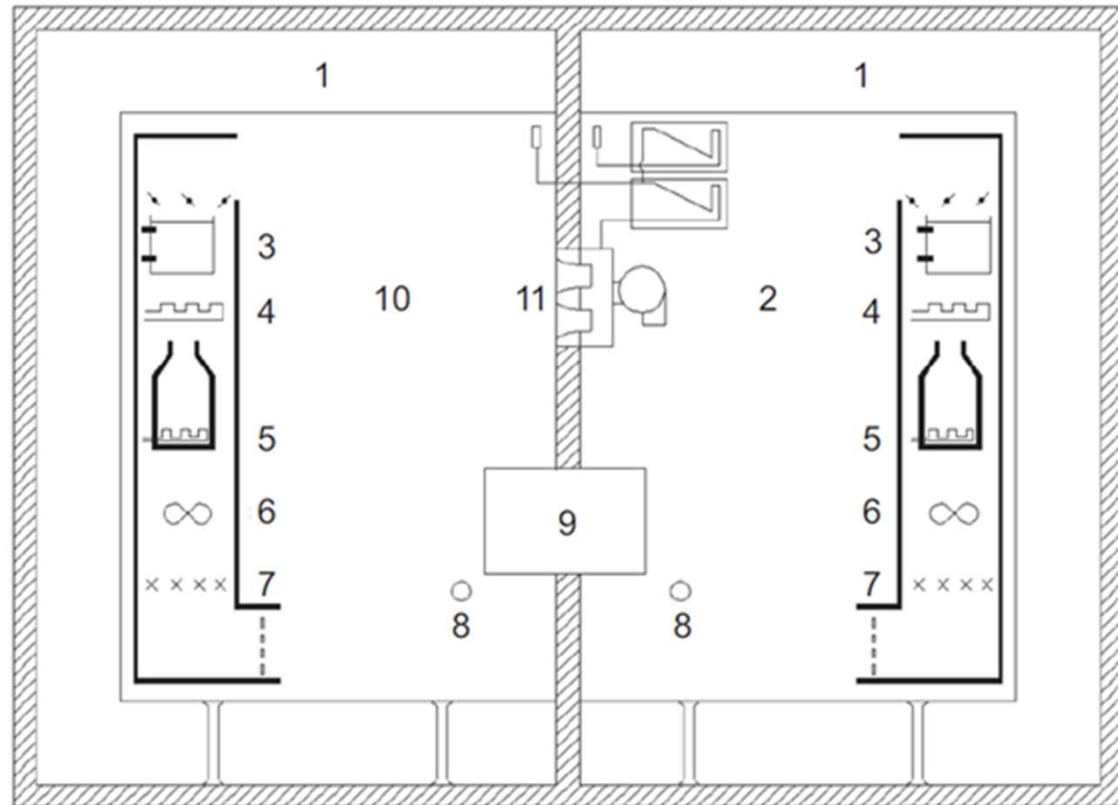
Part 3: Test methods

Part 4: Requirements

Balanced calorimeter room method

Raised view of a Balanced calorimeter

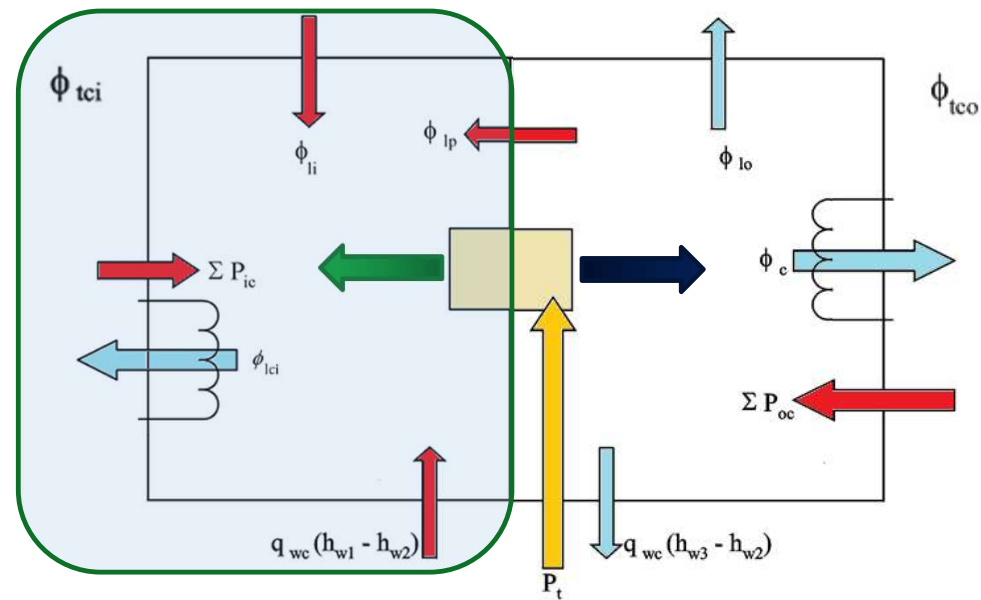
- 1 controlled-temperature air space
- 2 outdoor-side compartment
- 3 cooling coil
- 4 heating coil
- 5 humidifier
- 6 fan
- 7 mixer
- 8 air sampling tube
- 9 equipment under test
- 10 indoor-side compartment
- 11 pressure equalization device



Balanced calorimeter room method



Balanced calorimeter room method

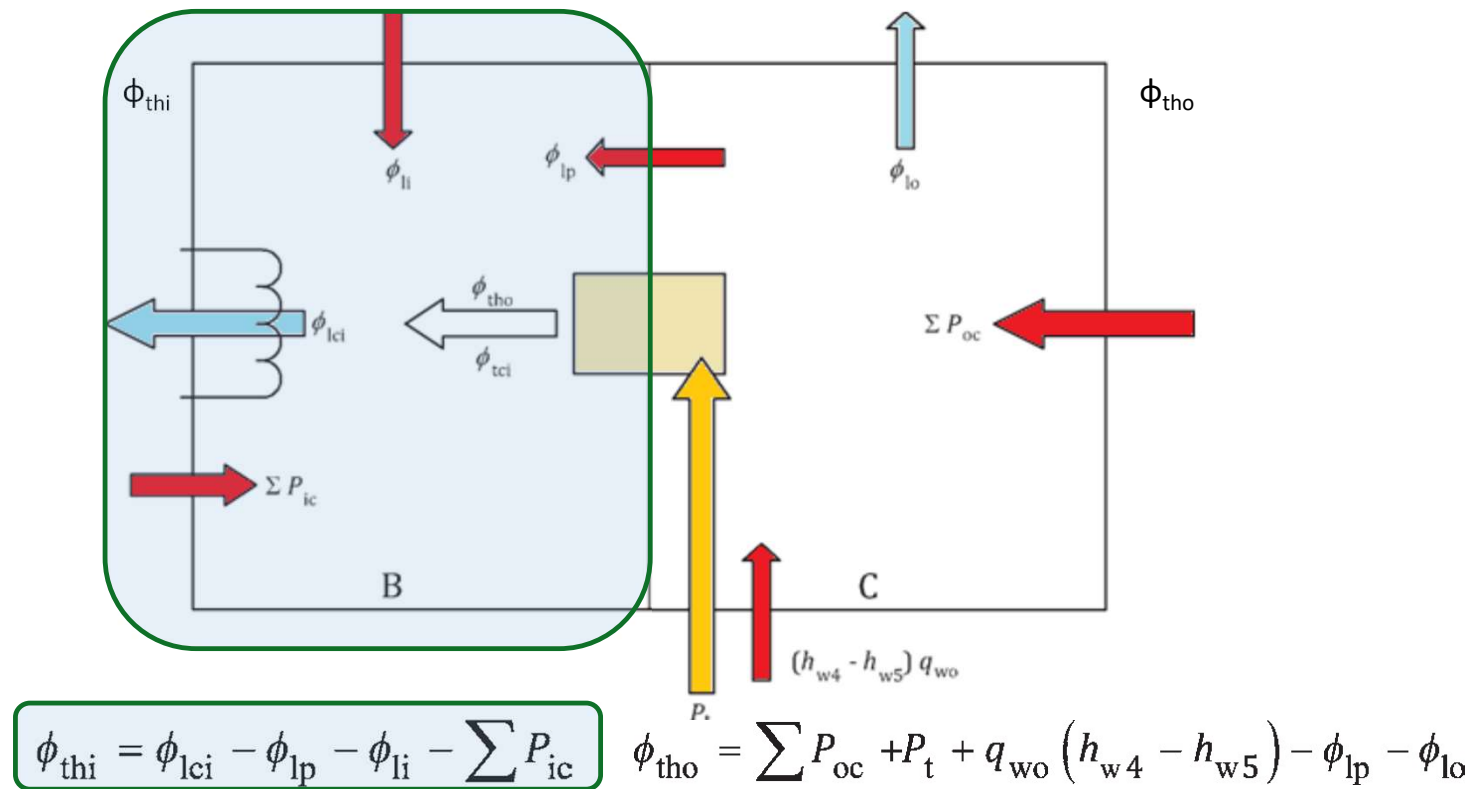


$$\phi_{tci} = \sum P_{ic} + q_{wc}(h_{w1} - h_{w2}) + \phi_{lp} + \phi_{li} - \phi_{lci}$$

$$\phi_{tco} = \phi_c - \sum P_{oc} - P_t + q_{wc}(h_{w3} - h_{w2}) + \phi_{lp} + \phi_{lo}$$

Energy flows during Cooling capacity measurement

Balanced calorimeter room method



Energy flows during Heating capacity measurement

Indoor Air enthalpy test method





40kW Rooftop UUT ready for capacity testing

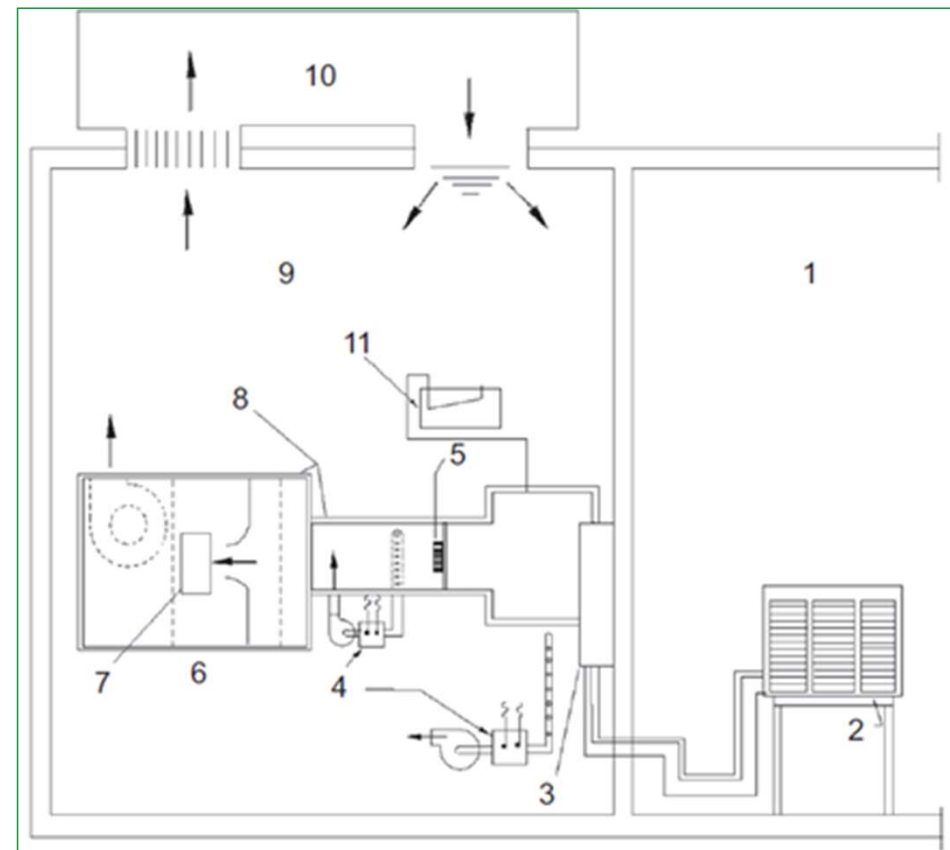
30kW total cooling capacity system set-up with 4 indoor ducted units



Indoor Air enthalpy test method

Raised view of an air enthalpy test room

- 1 outdoor-side test room
- 2 outdoor unit of equipment under test
- 3 indoor-side coil section of equipment under test
- 4 air temperature and humidity measuring instruments
- 5 mixer
- 6 airflow measuring apparatus
- 7 door/window
- 8 insulation
- 9 indoor-side test room
- 10 room conditioning apparatus
- 11 apparatus for differential pressure measurement



EN 14825:2022

Air conditioners, liquid chilling packages and heat pumps, with electrically driven compressors, for space heating and cooling, commercial and process cooling.

Testing and rating at part load conditions and calculation of seasonal performance.

SCOPE

- **Air conditioners, heat pumps and liquid chillers, including comfort and process chilelrs**
- The document specifies the temperatures, part-load conditions and calculation methods for determining the seasonal energy efficiency **SEER** and SEERon, the seasonal space cooling energy efficiency **$\eta_{s,c}$** , the seasonal coefficient of performance **SCOP**, SCOPon and SCOPnet, the seasonal space heating energy efficiency **$\eta_{s,h}$** and the seasonal energy coefficient of performance SEPR. This document also applies to the hybrid units defined in this standard
- It applies to factory-made units as defined in EN 14511-1, except single-duct, double-duct, control cabinet and close control units. It also covers direct exchange heat pumps with water (brine) (DX with water (brine)) as defined in EN 15879-1
- Also applies to hybrid units as defined in the standard

Basic concepts I

Reference design conditions

- **Cooling mode ($T_{designc}$)** → **$P_{designc}$**

Outdoor temperature is 35 °C DB

-> For air-to-air units 24 °C WB required for units evaporating the condensate

Indoor temperature of 27 °C DB (19 °C WB)

- **Heating mode ($T_{designh}$)** → **$P_{designh}$**

Three climatic areas have been defined: Average, colder and warmer.

Design temperature conditions are as follows:

- **Average climate:** Outdoor temperature is -10 °C DB (-11°C WB) and indoor temperature is 20 °C DB
- **Colder climate:** Outdoor temperature is -22°C DB and indoor temperature is 20 °C DB
- **Warmer climate:** Outdoor temperature is +2°C DB and indoor temperature is 20 °C DB

Basic concepts II

Declared conditions

- **Bivalent temperature (T_{bivalent})**

lowest outdoor temperature for which the heat pump is declared to have the capacity to compensate 100% of the heat load

- for the **average climate**, it is **+2°C BS or lower**
- for **colder climate**, it is **-7°C BS or lower**
- for **warmer climate**, it is **+7°C BS or lower**

- **Temperature Operating Limit (TOL)**

lowest outdoor temperature for which it is declared that the heat pump is still able to deliver heating capacity

- for the **average climate**, it is **-7°C BS or below**
- for **colder climate**, it is **-15°C BS or below**
- for **warmer climate**, it is **+7°C BS or below**

Basic concepts III

- **Operating modes**

- Active: when there is thermal load and the cooling or heating function of the unit remains active (compressor ON).
- Standby mode: Waiting for input from the user
- Thermostat off mode: Compressor is off because room target conditions are already achieved
- Power Off mode: unit is disconnected from the power supply
- Crankcase heater mode: electrical heater may be ON under certain circumstances

} Non-active modes

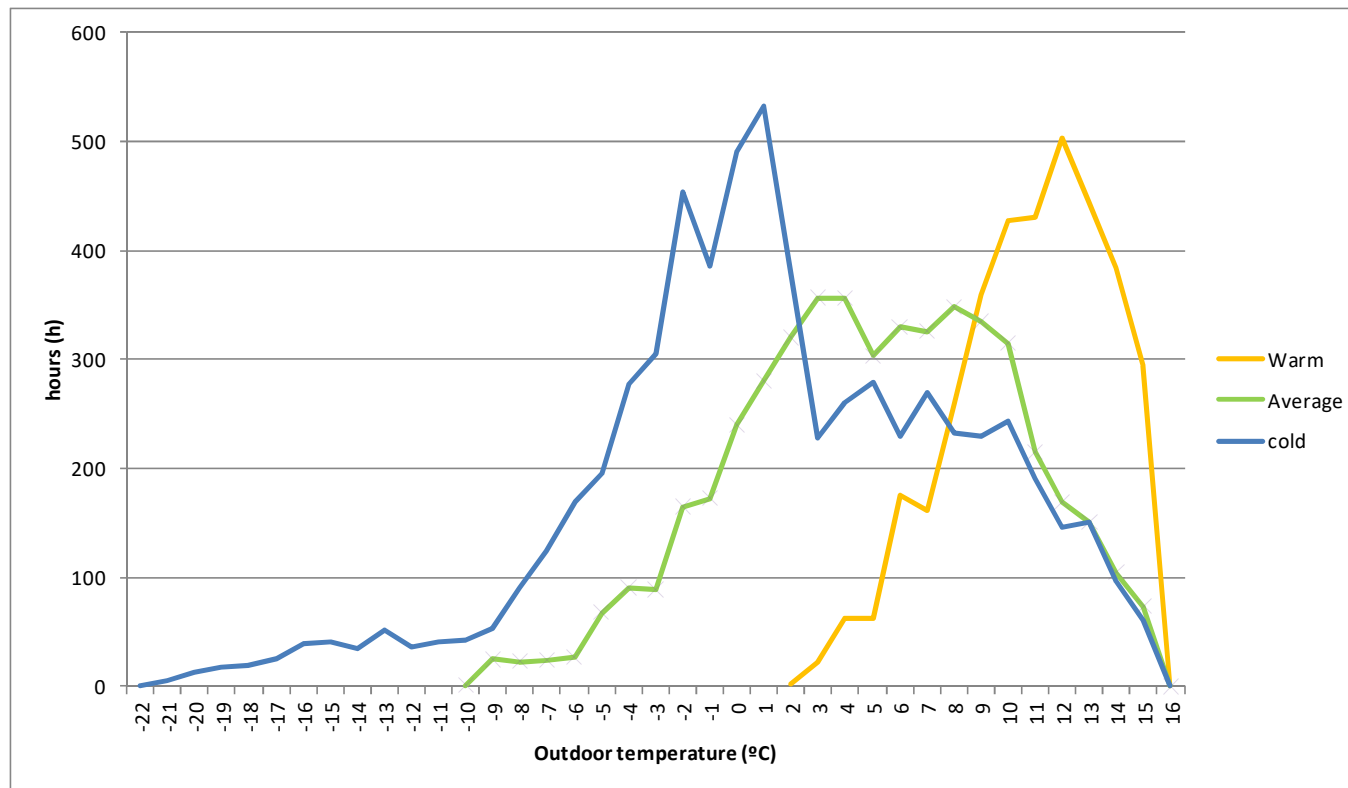
- **Table bin**

- Table describing the climate based on the outdoor temperature and the number of hours of occurrence in the season.

j	#	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
T_j	°C	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40
h_j	h	205	227	225	225	216	215	218	197	178	158	137	109	88	63	39	31	24	17	13	9	4	3	1	0

} Reference bin table for air-to-air units
(Hot season - cooling mode)

Basic concepts IV



Climate definitions for the cold season

Basic concepts V

THERMAL LOAD in COOLING and HEATING modes

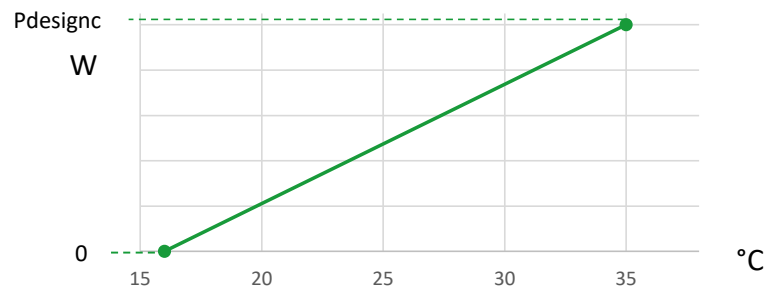
- Also referred to as building thermal load or building thermal demand
- Straight line defined from:
 - Thermal load = 0 at 16°C (from definition)

&

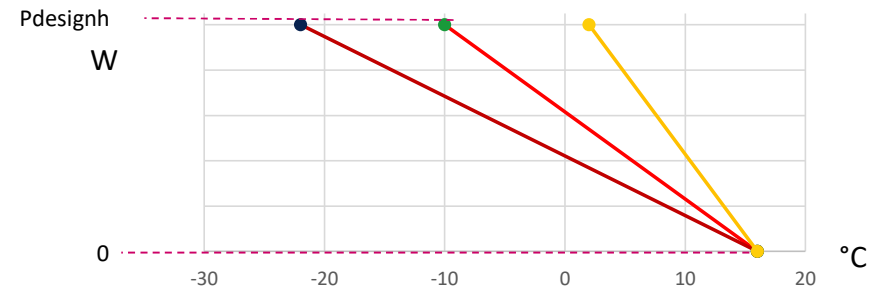
For cooling mode:
Thermal load = $P_{designc}$ at 35°C

For heating mode:
Thermal load = $P_{designh}$ at -10°C, -22°C or 2°C.

Demand in cooling mode & $P_{designc}$



Demand in heating mode & $P_{designh}$



Seasonal Space cooling & heating efficiency

$$\eta_{s,c} = \frac{SEER}{CC} - F1 - F2 ; \eta_{s,h} = \frac{SCOP}{CC} - F1 - F2$$

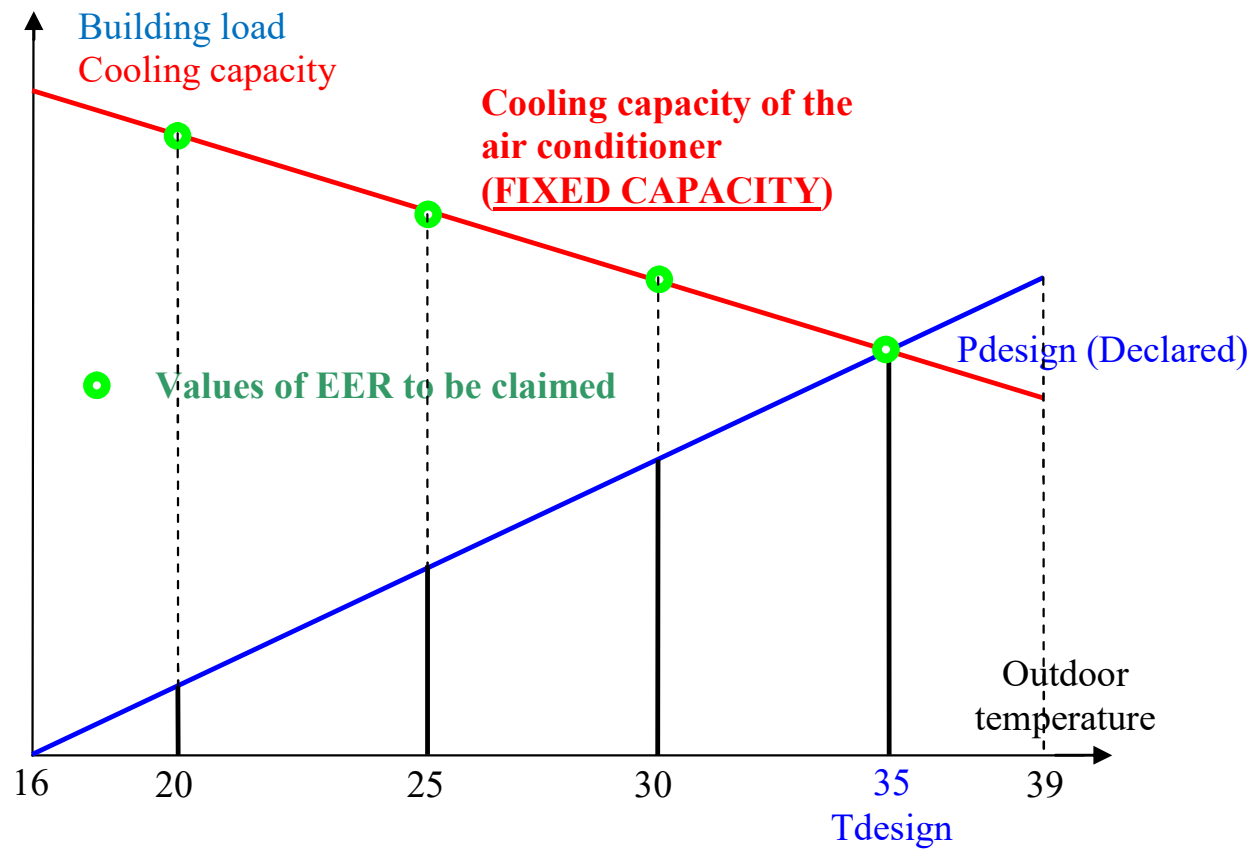
- CC is the primary energy correction coefficient to refer electricity consumption to the average efficiency of electricity generation in Europe
- The CC value must be checked in the product regulations
- F1 is a correction factor that takes into account inefficiencies due to thermostat management (3%)
- F2 is a correction factor that takes into account the effect of groundwater circulation pumps (5%)

Test Conditions

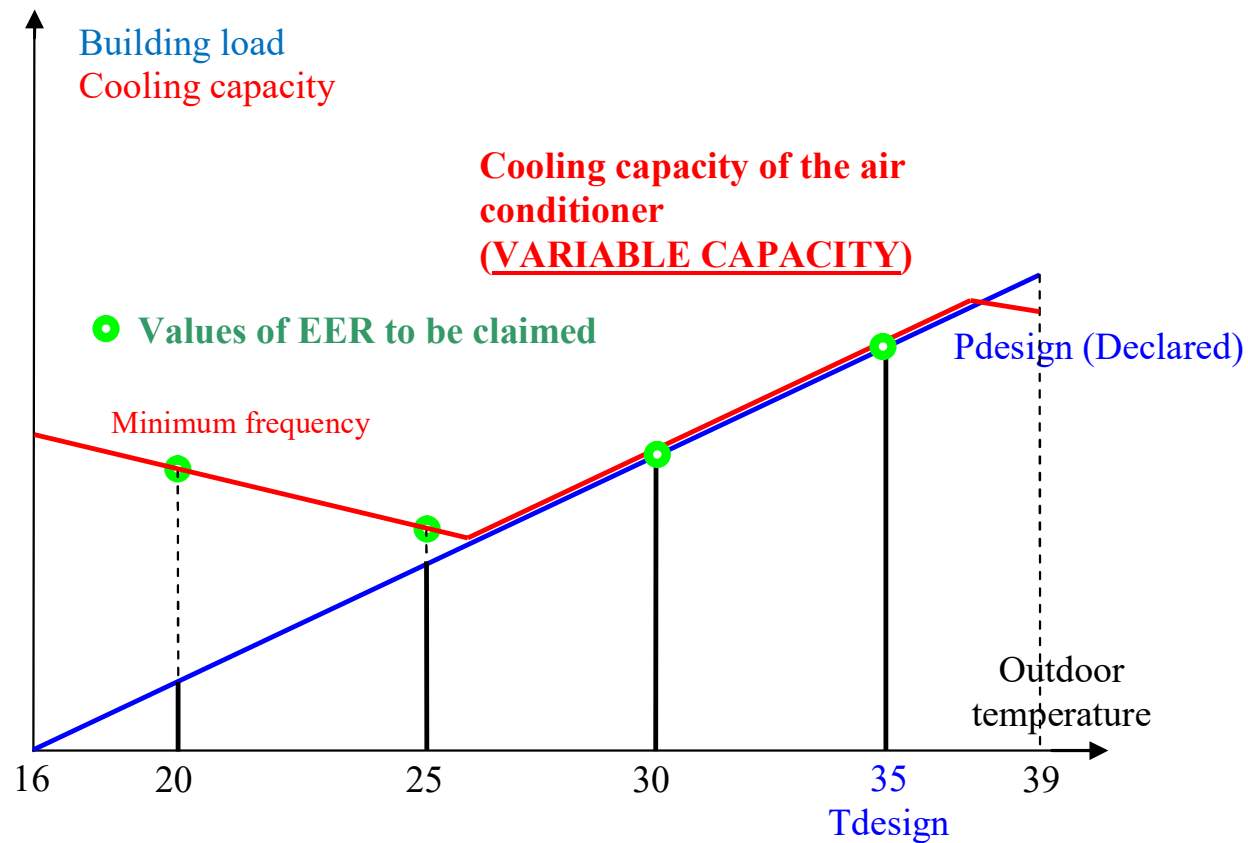
- Air/air units

	Part load	Part load	Outdoor air dry bulb temperature	Indoor air Dry bulb (wet bulb) temperatures
		%	°C	°C
A	$(35-16)/(T_{\text{designc}}-16)$	100	35	27(19)
B	$(30-16)/(T_{\text{designc}}-16)$	73,68	30	27(19)
C	$(25-16)/(T_{\text{designc}}-16)$	47,37	25	27(19)
D	$(20-16)/(T_{\text{designc}}-16)$	21,05	20	27(19)

Cooling capacity and thermal load for On/Off unit



Cooling capacity and thermal load for variable capacity unit



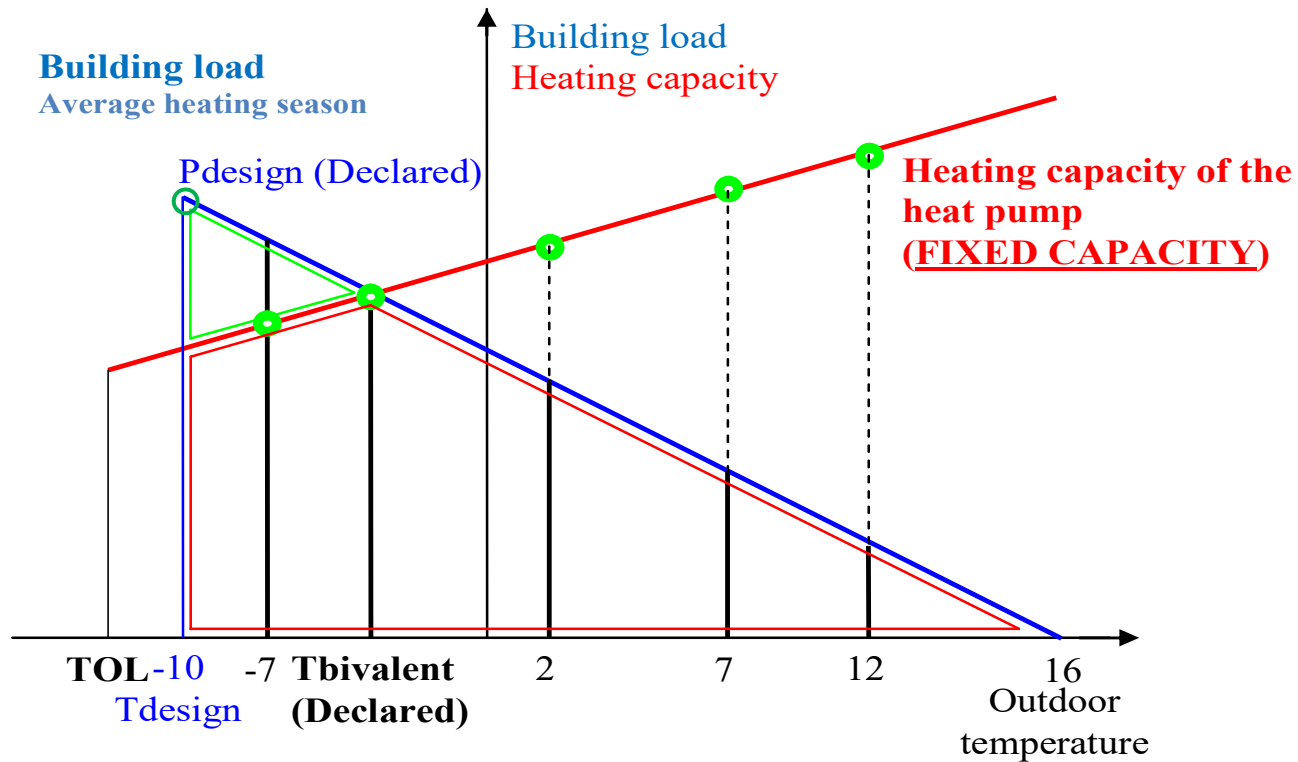
Test Conditions

- Air-to-air units

	Partial load in % of load				Outdoor heat exchanger	Internal heat exchanger
	Part load	Average	Warmer	Colder	Dry(wet) bulb temperatures °C	Dry bulb temperature °C
A	$\frac{(-7 - 16)}{(T_{designh} - 16)}$	88,46	n/a	60,53	-7(-8)	20
B	$\frac{(+2 - 16)}{(T_{designh} - 16)}$	53,85	100	36,84	2(1)	20
C	$\frac{(+7 - 16)}{(T_{designh} - 16)}$	34,62	64,29	23,68	7(6)	20
D	$\frac{(+12 - 16)}{(T_{designh} - 16)}$	15,38	28,57	10,53	12(11)	20
E	$(TOL^a - 16) / (T_{designh} - 16)$				TOL	20
F	$(T_{bivalent} - 16) / (T_{designh} - 16)$				Tbivalent	20
G	$\frac{(-15 - 16)}{(T_{designh} - 16)}$	n/a	n/a	81,58	-15	20

^a If TOL < Tdesignh replace TOL by Tdesignh

Heating capacity and Heat load for On/Off unit

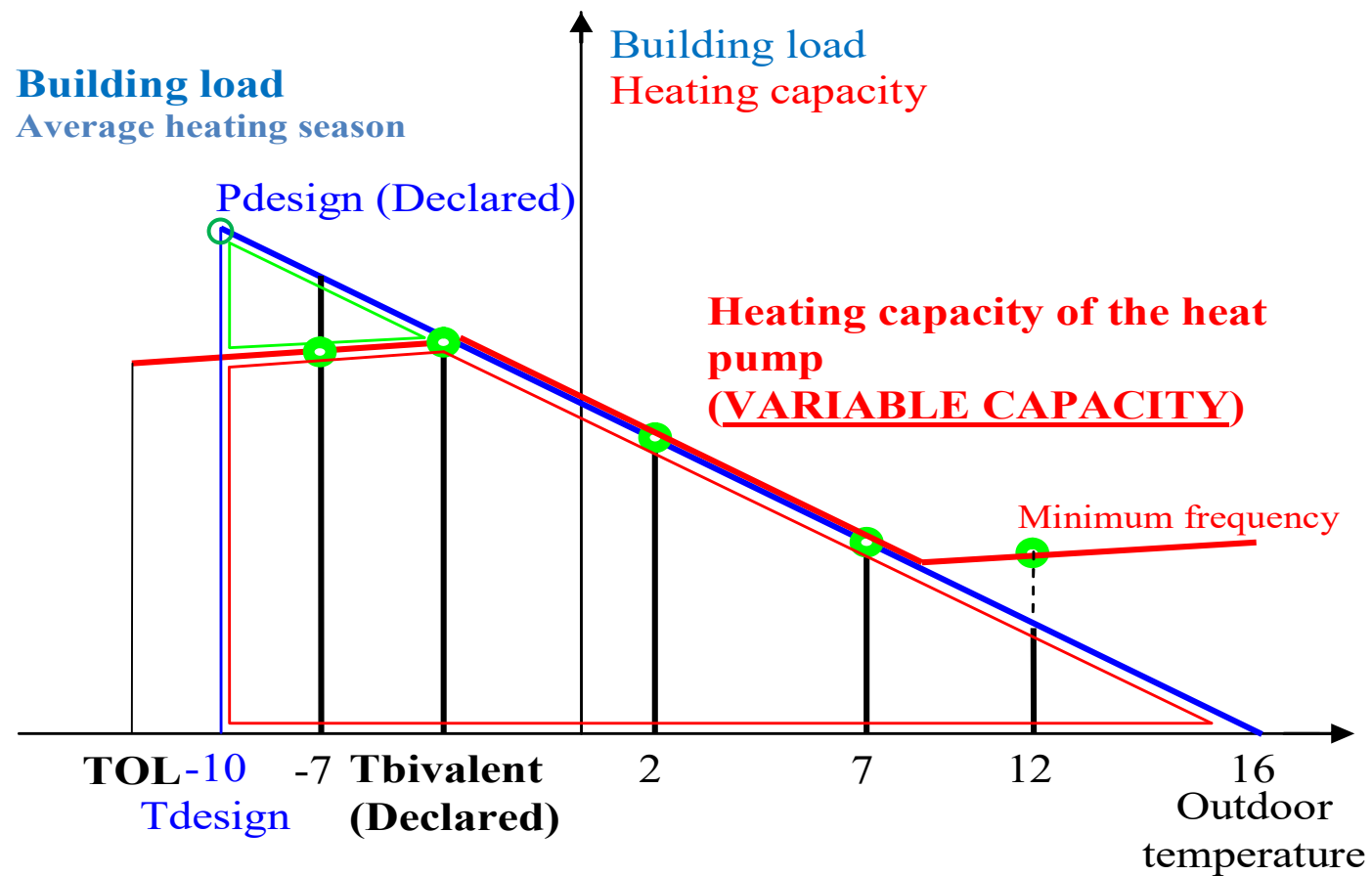


● Values of COP to be claimed

□ Heating needs covered by the heat pump

□ Heating needs covered by an electrical heater COP = 1

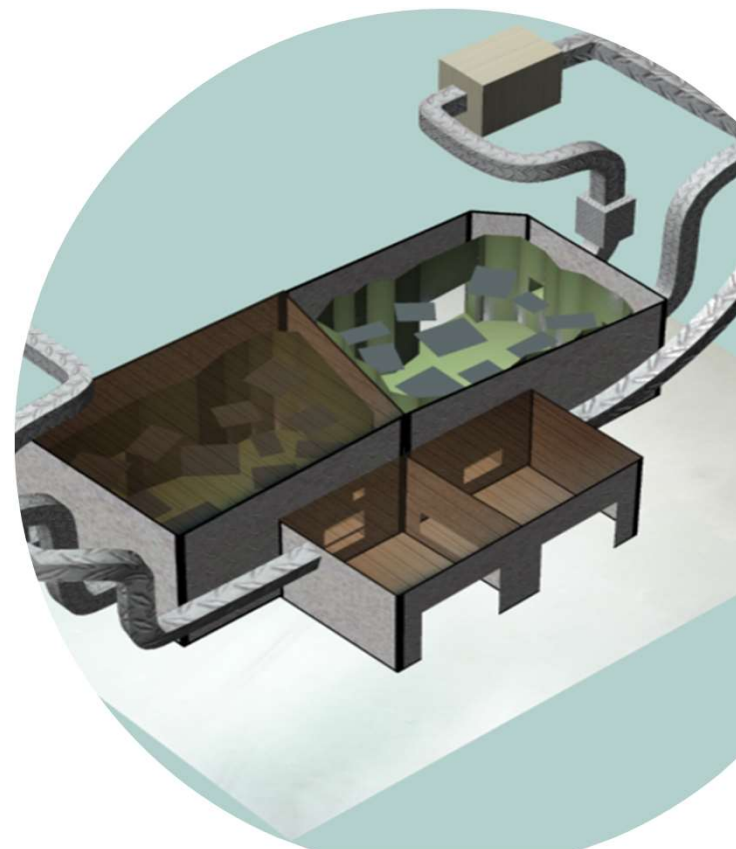
Heating capacity and Heat load for variable capacity unit



EN 12102-1:2022

Air conditioners, liquid chilling packages, heat pumps, process chillers and dehumidifiers with electrically driven compressors.

Determination of the sound power level Air conditioners, liquid chilling packages, heat pumps for space heating and cooling, dehumidifiers and process chillers



Sound pressure and Sound power

□ Sound pressure

The sound pressure, p (Pa) is defined as the instantaneous pressure difference due to noise (fluctuating) and the atmospheric pressure.
It depends on the sound source and environment of the sound source (location set-up)

□ Sound power

The Sound power P (W) is the amount of acoustic energy radiated by a noise source. This is dependent on the noise source and independent from noise source location or distance at which the sound power is measured



Both parameters are usually expressed in dB or dB(A)

The dB reference for sound pressure is $P_0 = 20 \cdot 10^{-6}$ Pa = 20 μ Pa $\rightarrow L_P = 20 \cdot \text{Log} \frac{P}{P_0}$

The dB reference for sound power is $W_0 = 10 \cdot 10^{-12}$ W = 1 pW $\rightarrow L_W = 10 \cdot \text{Log} \frac{W}{W_0}$

EN 12102-1:2022 + EN ISO 3741:2010

Direct test method

Sound power is obtained from measurements of sound pressure level in the reverberant sound field and Sabine's absorption coefficient of the room with the unit under test installed in the test room.

Comparison method

Sound power is obtained from comparison between the sound pressure levels in the room from the unit under test and a Reference Sound Source (RSS)

**Allowed test methods in EN 12102-1 are developed in:*

EN ISO 3741

EN ISO 3742

- Reverberant rooms

EN ISO 3744

EN ISO 3745

- Free field conditions

EN ISO 9614 series

- Intersimetry

EN 12102-1:2022 + EN ISO 3741:2010

- Depending on the selected test method, we measure in the third octave range from 100Hz to 10,000Hz or from 100Hz to 6,300Hz (intensimetry methods)

Example of results for an equipment with VPD > 10

1/3 Octave	Final Result [dB]	
100Hz	47,5	51,2
125Hz	42,6	
160Hz	47,5	
200Hz	50,8	56,2
250Hz	48,0	
315Hz	53,6	
400Hz	50,9	56,6
500Hz	51,8	
630Hz	52,5	
800Hz	52,7	56,7
1kHz	52,0	
1.25kHz	50,9	
1.6kHz	50,3	53,7
2kHz	48,8	
2.5kHz	47,2	
3.15kHz	46,6	50,0
4kHz	45,0	
5kHz	43,7	
6.3kHz	40,4	44,5
8kHz	40,1	
10kHz	38,4	
Global	62,6	62,6

EN 16147:2017 + AC1:2017

Heat pumps with electrically driven compressors - Testing, performance rating and requirements for marking of domestic hot water units.

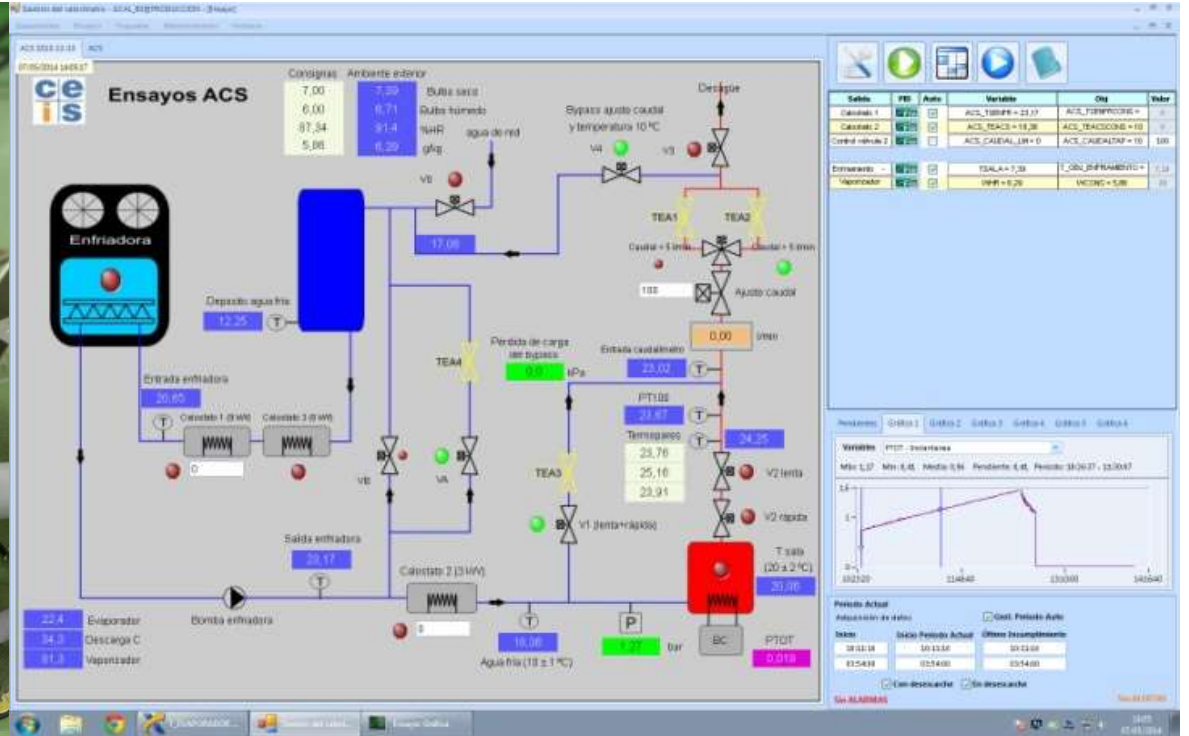
Scope

- *Air-to-water, water(brine)-to-water and direct exchange heat pumps (DX)*
- *Only applies to DHW heat pumps rated as a single system, including a heat pump and a hot water storage tank*

EN 16147:2017 + AC1:2017



EN 16147:2017 + AC1:2017



EN 16147:2017 + AC1:2017

☐ Test conditions

Type of heat source	Heat source Dry bulb(wet bulb) air temperature in °C	Heat source Inlet/outlet or bath temperature ^a in °C	Heat pump ambient temperature range in °C	Ambient temperature for storage tank in °C
Outdoor air-source heat pump (located indoors)				
Average	7 (6)	-	between 15 and 30	20
Colder	2 (1)			
Warmer	14 (13)			
Outdoor air-source heat pump (located outdoors)				
Average	7 (6)	-	temperature of the heat source	20
Colder	2 (1)			
Warmer	14 (13)			
Unheated air space	15 (12)	-	temperature of the heat source	15
Indoor air	20 (15)	-	temperature of the heat source	20
Extracted air	20 (12)	-	between 15 and 30	20
Water	-	10 / 7	between 15 and 30	20
Glycol water (brine)	-	0 / -3	between 15 and 30	20
Direct expansion	-	4	between 15 and 30	20

EN 16147:2017 + AC1:2017

Test Stages

Stage B Filling and volume of the storage tank

Only for units within EU 814/2013 scope up S tapping cycle only

Stage A Stabilisation (preconditioning)

Stage C Warm-up period

Stage D Steady state power consumption

Stage E Water tapping and COP determination

Stage F Mixed water at 40°C and reference hot water temperature

EN 16147:2017 + AC1:2017

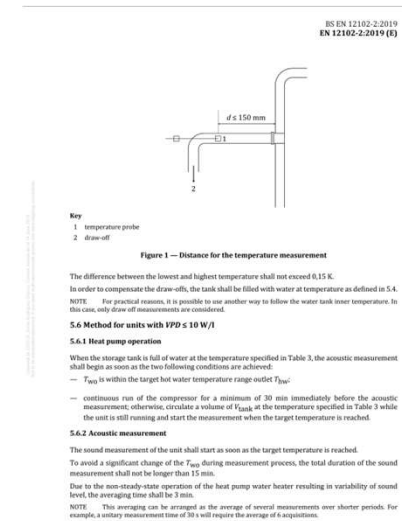
□ Test results from Stages B,C,D And F allows to calculate:

- Hot water tank Heat-up time
- Standby power input (= $P_{es} \cdot CC$)
- **Qelec***
- COPDHW for the use profile declared by the manufacturer
- **Tank volume***
- **V40 (mixed water at 40°C)***
- Reference temperature (required by the French regulation only)
- AEC - Annual energy consumption
- **η_{wh} - Water heater energy efficiency***
- Prated - Declared heating power

*Checked during market surveillance

EN 12102-2:2019

Air conditioners, liquid chilling packages, heat pumps, process chillers and dehumidifiers with electrically driven compressors - Determination of the sound power level - Part 2: Heat pump water heaters



- It establish the test methods to determine the sound power level for DHW products

EN 12102-2:2019 + EN ISO 3741:2010



- 3 different test methods
- The method depends on the VPD (volumic power density)
- VPD relates to the hot water tank heat-up speed and thus,
- How fast the running parameters of the heat pump change accross time.

EN 12102-2:2019 + EN ISO 3741:2010

☐ The test is carried out under a permanently transient regime.

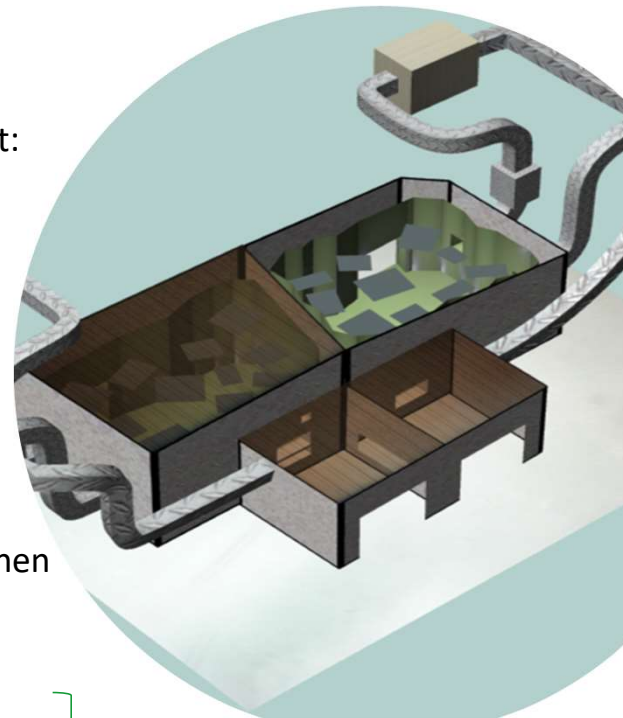
3 test procedures defined according to the *type* of equipment:

- VPD value ≤ 10
- VPD value > 10
- Direct cold water expansion (CO2 equipment)

VPD - Volumetric Power Density

$$VPD = \frac{P_{rated}}{V_{tank}} \cdot 1000$$

☐ The test consists of determining the sound power levels when certain temperatures are reached in the DHW tank (Thw).



T_{hw}	25°C	}	VPD
	$(T_{SET} + 25)/2$ °C		
	$(T_{SET} - 5)$ °C		

$$\frac{T_{wo} - T_{start}}{T_{set} - T_{start}} \times D_H$$

}	T _{wo}	Final hot water temperature
	D _H	Duration of warm-up
	T _{start}	Initial DHW tank temperature (10±2K)
	T _{set}	DHW storage tank setpoint temperature

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Together We Switch to Clean Energy

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Annex I

Equations from test methods in EN 14511-3:2022

Indoor Air enthalpy test method

Total cooling capacity

$$\phi_{tci} = \frac{q_{vi} (h_{\alpha 1} - h_{\alpha 2})}{v'_n (1 + W_n)} 1\,000$$

Sensible capacity

$$\phi_s = \frac{q_{vi} (c_{pa1} t_{a1} - c_{pa2} t_{a2})}{v'_n (1 + W_n)}$$

Latent capacity

For the cooling mode, it is recommended that the latent cooling capacity be determined using the cooling condensate flow rate measurement method.

$$\phi_d = \frac{K_1 q_{vi} (W_{i1} - W_{i2})}{v'_n (1 + W_n)} 1000$$

$$\phi_d = K_1 q_{wc}$$

$$\phi_d = \phi_{tci} - \phi_s$$

Key	
qvi= Volumetric air flow rate (m ³ /s)	v'n= specific air volume (m ³ /kg)
K1 = Water vapour latent heat of vaporization = 2500,4 J/g at 0°C	h = air enthalpy (kJ/kg)
qwc = condensate waterflow rate (kg/s)	Wi(1,2) = specific humidity of air entering(1)/leaving(2) the indoor unit's coil ((kg of water / kJ of dry air)

Indoor Air enthalpy test method

Heating capacity

$$\phi_{thi} = \frac{q_{vi}(h_{a2} - h_{a1})}{v'_n (1 + W_n)}$$

$$\phi_{thi} = \frac{q_{vi}(c_{pa2} \times t_{a2} - c_{pa1} \times t_{a1})}{v_n} = \frac{q_{vi}(c_{pa2} \times t_{a2} - c_{pa1} \times t_{a1})}{v'_n \times (1 + W_n)}$$

Key	
qvi= Volumetric air flow rate (m ³ /s)	v'n= specific air volume (m ³ /kg)
h = air enthalpy (kJ/kg)	Wn = specific humidity at nozzles section (kg of water / kg of dry air)
Cp = specific heat of air	t = air temperature (dry bulb)

Indoor water enthalpy test method

Cooling capacity

$$\phi_{tci} = -q_v \times \rho \times (c_{p_out} \times t_{out} - c_{p_in} \times t_{in})$$

Heating capacity

$$\phi_{thi} = q_v \times \rho \times (c_{p_out} \times t_{out} - c_{p_in} \times t_{in})$$

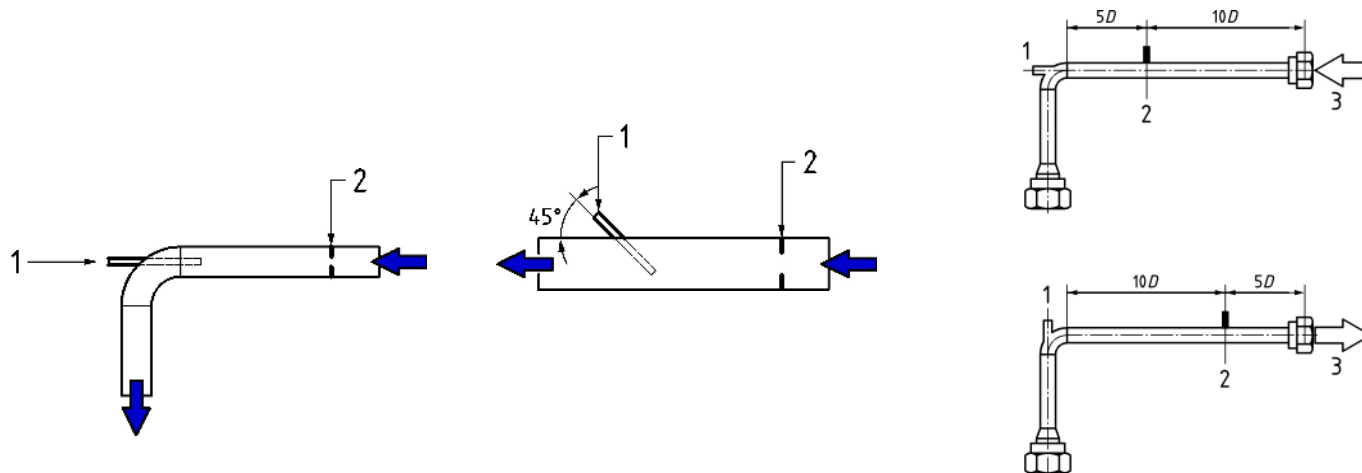
Key

q_v = Volumetric water flow rate (m³/s)

ρ = Water density (kg/m³)

C_p = specific heat of water (kJ/(kg/°C))

t = water temperature (dry bulb) (°C)



Annex II

Test conditions from EN 14825 in cooling mode

Test conditions for cooling mode

- Air-to-air units

	Part load	Part load	Outdoor air dry bulb temperature	Indoor air Dry bulb (wet bulb) temperatures
		%	°C	°C
A	$(35-16)/(T_{\text{designc}}-16)$	100	35	27(19)
B	$(30-16)/(T_{\text{designc}}-16)$	73,68	30	27(19)
C	$(25-16)/(T_{\text{designc}}-16)$	47,37	25	27(19)
D	$(20-16)/(T_{\text{designc}}-16)$	21,05	20	27(19)

Test conditions for cooling mode

- Water-to-air units

	Part load	Part load	Outdoor heat exchanger			Indoor heat exchanger
			Cooling tower or water loop ^b Water inlet and outlet temperatures	Geothermal (water or brine) Water inlet and outlet temperatures	Dry cooling Water inlet and outlet temperatures	Dry bulb temperature (wet bulb) indoor air
			%	°C	°C	°C
A	$(35-16)/(T_{designc} - 16)$	100	30 / 35	10 / 15	50 / 55	27(19)
B	$(30-16)/(T_{designc} - 16)$	73,68	26 / ^a	10 / ^a	45 / ^a	
C	$(25-16)/(T_{designc} - 16)$	47,37	22 / ^a	10 / ^a	40 / ^a	
D	$(20-16)/(T_{designc} - 16)$	21,05	18 / ^a	10 / ^a	35 / ^a	

^a Water flow rate as determined in the "A" test.

^b If a cooling tower and a water-air unit are sold as a set, they must be tested as one air-air unit.

Test conditions for cooling mode

- Air-to-water units

	Part load	Part load	Outdoor heat exchanger		Indoor heat exchanger		
			Dry bulb outside air	Dry bulb exhaust air	Fan coil application		Application Refrigerated floor
					Water temperatures (brine) Inlet/Outlet		Water temperatures (brine) Inlet/Outlet
					Fixed output	Variable output ^b	
	%	°C	°C	°C	°C	°C	
A	$(35-16)/(T_{designc} - 16)$	100	35	27	12 / 7	12 / 7	23 / 18
B	$(30-16)/(T_{designc} - 16)$	73,68	30	27	^a / 7	^a / 8,5	^a / 18
C	$(25-16)/(T_{designc} - 16)$	47,37	25	27	^a / 7	^a / 10	^a / 18
D	$(20-16)/(T_{designc} - 16)$	21,05	20	27	^a / 7	^a / 11,5	^a / 18

^a With the water flow rate determined during test "A" for units with fixed flow rate or with 5K temperature difference for units with variable flow rate. If in a test condition the resulting flow rate is less than the minimum allowed by the unit, then the minimum flow rate and the required outlet temperature is used.

^b If the variable output temperature is above the maximum output temperature (of the unit), the maximum value allowed by the unit is used.

Test conditions for cooling mode

- Water(brine)-to-water(brine) units

	Part load	Part load	Outdoor heat exchanger				Internal heat exchanger		
			Cooling tower or water loop (brine) Inlet/outlet temperatures of water (brine)	Geothermal application Inlet/outlet water temperatures (brine)	Dry cooler application Inlet/outlet water (brine) temperatures	DX Bath temperature	Fan coil application		Application Refrigerated floor
							Water temperatures (brine) Inlet/Outlet		Water temperatures (brine) Inlet/Outlet
							Fixed output	Variable output ^b	
	%	°C	°C	°C	°C	°C	°C	°C	
A	(35-16)/ (T _{designc} - 16)	100	30 / 35	10 / 15	50 / 55	30	12 / 7	12 / 7	23 / 18
B	(30-16)/ (T _{designc} - 16)	73,68	26 / ^b	10 / ^b	45 / ^b	30	^a / 7	^a / 8,5	^a / 18
C	(25-16)/ (T _{designc} - 16)	47,37	22 / ^b	10 / ^b	40 / ^b	30	^a / 7	^a / 10	^a / 18
D	(20-16)/ (T _{designc} - 16)	21,05	18 / ^b	10 / ^b	35 / ^b	30	^a / 7	^a / 11,5	^a / 18

^a With the water flow rate determined during test "A" for units with fixed flow rate or with 5K temperature difference for units with variable flow rate. If in a test condition the resulting flow rate is less than the minimum, then the minimum flow rate and the required outlet temperature is used.

^b With the water flow rate determined during test "A" for units with fixed flow rate or with 5K temperature difference for units with variable flow rate. If in a test condition the resulting flow rate is less than the minimum, then the minimum flow rate and the required inlet temperature is used.

^c If the variable output temperature is above the maximum output temperature (of the unit), the maximum value allowed by the unit is used.

Annex II

Test conditions from EN 14825 in Heating mode

Test Conditions

- Air-to-air units

	Partial load in % of load				Outdoor heat exchanger	Internal heat exchanger
	Part load	Average	Warmer	Colder	Dry(wet) bulb temperatures °C	Dry bulb temperature °C
A	$\frac{(-7 - 16)}{(T_{designh} - 16)}$	88,46	n/a	60,53	-7(-8)	20
B	$\frac{(+2 - 16)}{(T_{designh} - 16)}$	53,85	100	36,84	2(1)	20
C	$\frac{(+7 - 16)}{(T_{designh} - 16)}$	34,62	64,29	23,68	7(6)	20
D	$\frac{(+12 - 16)}{(T_{designh} - 16)}$	15,38	28,57	10,53	12(11)	20
E	$(TOL^a - 16) / (T_{designh} - 16)$				TOL	20
F	$(T_{bivalent} - 16) / (T_{designh} - 16)$				Tbivalent	20
G	$\frac{(-15 - 16)}{(T_{designh} - 16)}$	n/a	n/a	81,58	-15	20

^a If TOL < Tdesignh replace TOL by Tdesignh

Test conditions for heating mode

- Water(brine)-to-air units

	Part load				Outdoor heat exchanger			Indoor heat exchanger
	%				Input/output temperatures			
	Formula	Average	Warmer	Colder	Water °C	Brine °C	Water loop °C	Dry bulb °C
A	$(-7 - 16) / (T_{\text{designh}} - 16)$	88,46	n.a.	60,53	10 / ^a	0 / ^a	20/ ^a	20
B	$(+2 - 16) / (T_{\text{designh}} - 16)$	53,85	100	36,84	10 / ^a	0 / ^a	20/ ^a	20
C	$(+7 - 16) / (T_{\text{designh}} - 16)$	34,62	64,29	23,68	10 / ^a	0 / ^a	20/ ^a	20
D	$(+12 - 16) / (T_{\text{designh}} - 16)$	15,38	28,57	10,53	10 / ^a	0 / ^a	20/ ^a	20
E	$(TOL^b - 16) / (T_{\text{designh}} - 16)$				10 / ^a	0 / ^a	20/ ^a	20
F	$(T_{\text{biv}} - 16) / (T_{\text{designh}} - 16)$				10 / ^a	0 / ^a	20/ ^a	20

a With the water flow rate determined at the standard conditions given in table 5 of EN 14511-2:2018 for fixed flow units or with a temperature difference of 3K for variable flow units. If in any test condition the required flow rate is lower than the minimum flow rate of the unit, the minimum flow rate with the inlet temperature for that condition is used.

b If $TOL < T_{\text{designh}}$ replace TOL by T_{designh}

Test conditions for heating mode

- Air-to-water(brine) units -Low temperature application

	Partial Load				Outdoor heat exchanger		Indoor heat exchanger			
	%				Dry Bulb (Wet Bulb) temperatures		Fixed output	Variable Output ^d		
					°C			°C	°C	
	Formula	Average	Warmer	Colder	Outdoor air	Exhaust air		Average	Warmer	Colder
A	$(-7 - 16) / (T_{designh} - 16)$	88,46	n.a.	60,53	-7(-8)	20(12)	^a / 35	^a / 34	n.a.	^a / 30
B	$(+2 - 16) / (T_{designh} - 16)$	53,85	100	36,84	2(1)	20(12)	^a / 35	^a / 30	^a / 35	^a / 27
C	$(+7 - 16) / (T_{designh} - 16)$	34,62	64,29	23,68	7(6)	20(12)	^a / 35	^a / 27	^a / 31	^a / 25
D	$(+12 - 16) / (T_{designh} - 16)$	15,38	28,57	10,53	12(11)	20(12)	^a / 35	^a / 24	^a / 26	^a / 24
E	$(TOL^e - 16) / (T_{designh} - 16)$				TOL ^e	20(12)	^a / 35	^a / ^b	^a / ^b	^a / ^b
F	$(T_{biv} - 16) / (T_{designh} - 16)$				T _{biv}	20(12)	^a / 35	^a / ^c	^a / ^c	^a / ^c
G	$(-15 - 16) / (T_{designh} - 16)$	n.a.	n.a.	81,58	-15	20(12)	^a / 35	n.a.	n.a.	^a / 32

^a With the flow rate determined at the nominal conditions in Table 12 of EN 14511-2:2018 at conditions 30/35 for fixed flow units, and with a water temperature difference of 5K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate for the unit, the minimum flow rate is used together with the outlet water temperature.

^b The variable outlet temperature is calculated by interpolation from T_{design} to the temperature closest to TOL.

^c The variable outlet temperature is calculated by interpolation from the temperatures immediately above and below T_{bivalent}.

^d If the output temperature is below the unit minimum, the unit minimum is used.

^e If TOL < T_{designh} then TOL is replaced by T_{designh}.

Test conditions for heating mode

- Air-to-water(brine) units - Intermediate temperature application

	Partial Load				Outdoor heat exchanger		Indoor heat exchanger			
	%				Dry Bulb (Wet Bulb) temperatures		Fixed output °C	Variable Output ^d		
					°C			°C		
	Formula	Average	Warmer	Colder	Outdoor air	Exhaust air		Average	Warmer	Colder
A	$(-7 - 16) / (T_{\text{designh}} - 16)$	88,46	n.a.	60,53	-7(-8)	20(12)	^a / 45	^a / 43	n.a.	^a / 38
B	$(+2 - 16) / (T_{\text{designh}} - 16)$	53,85	100	36,84	2(1)	20(12)	^a / 45	^a / 37	^a / 45	^a / 33
C	$(+7 - 16) / (T_{\text{designh}} - 16)$	34,62	64,29	23,68	7(6)	20(12)	^a / 45	^a / 33	^a / 39	^a / 30
D	$(+12 - 16) / (T_{\text{designh}} - 16)$	15,38	28,57	10,53	12(11)	20(12)	^a / 45	^a / 28	^a / 31	^a / 26
E	$(TOL^e - 16) / (T_{\text{designh}} - 16)$				TOL ^e	20(12)	^a / 45	^a / ^b	^a / ^b	^a / ^b
F	$(T_{\text{biv}} - 16) / (T_{\text{designh}} - 16)$				T _{biv}	20(12)	^a / 45	^a / ^c	^a / ^c	^a / ^c
G	$(-15 - 16) / (T_{\text{designh}} - 16)$	n.a.	n.a.	81,58	-15	20(12)	^a / 45	n.a.	n.a.	^a / 41

^a With the flow rate determined at the nominal conditions in Table 13 of EN 14511-2:2018 at conditions 40/45 for fixed flow units, and with a water temperature difference of 5K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate of the unit, the minimum flow rate is used together with the outlet water temperature.

^b The variable outlet temperature is calculated by interpolation from T_{design} to the temperature closest to TOL.

^c The variable outlet temperature is calculated by interpolation from the temperatures immediately above and below T_{bivalent}.

^d If the output temperature is below the unit minimum, the unit minimum is used.

^e If TOL < T_{designh} then TOL is replaced by T_{designh}.

Test conditions for heating mode

- Air-to-water units(brine) Medium temperature application

	Partial Load				Outdoor heat exchanger		Indoor heat exchanger			
	%				Dry Bulb (Wet Bulb) temperatures		Fixed output	Variable Output ^d		
					°C		°C	°C		
	Formula	Average	Warmer	Colder	Outdoor air	Exhaust air		Average	Warmer	Colder
A	$(-7 - 16) / (T_{designh} - 16)$	88,46	n.a.	60,53	-7(-8)	20(12)	^a / 55	^a / 52	n.a.	^a / 44
B	$(+2 - 16) / (T_{designh} - 16)$	53,85	100	36,84	2(1)	20(12)	^a / 55	^a / 42	^a / 55	^a / 37
C	$(+7 - 16) / (T_{designh} - 16)$	34,62	64,29	23,68	7(6)	20(12)	^a / 55	^a / 36	^a / 46	^a / 32
D	$(+12 - 16) / (T_{designh} - 16)$	15,38	28,57	10,53	12(11)	20(12)	^a / 55	^a / 30	^a / 34	^a / 28
E		$(TOL^e - 16) / (T_{designh} - 16)$			TOL ^e	20(12)	^a / 55	^a / ^b	^a / ^b	^a / ^b
F		$(T_{biv} - 16) / (T_{designh} - 16)$			T _{biv}	20(12)	^a / 55	^a / ^c	^a / ^c	^a / ^c
G	$(-15 - 16) / (T_{designh} - 16)$	n.a.	n.a.	81,58	-15	20(12)	^a / 55	n.a.	n.a.	^a / 49

^a With the flow rate determined at the nominal conditions in Table 14 of EN 14511-2:2018 at conditions 47/55 for fixed flow units, and with a water temperature difference of 8K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate of the unit then that minimum flow rate is used together with the outlet water temperature.

^b The variable outlet temperature is calculated by interpolation from T_{sedign} to the temperature closest to TOL.

^c The variable outlet temperature is calculated by interpolation from the temperatures immediately above and below T_{bivalent}.

^d If the output temperature is below the unit minimum, the unit minimum is used.

^e If TOL < T_{designh} then TOL is replaced by T_{designh}.

Test conditions for heating mode

- Air-to-water units(brine) High temperature application

	Partial Load				Outdoor heat exchanger		Temperatures heat exchanger			
	%				Dry Bulb (Wet Bulb) temperatures		Fixed output	Variable Output ^d		
					°C		°C	°C		
	Formula	Average	Warmer	Colder	Outdoor air	Exhaust air		Average	Warmer	Colder
A	$(-7 - 16) / (T_{designh} - 16)$	88,46	n.a.	60,53	-7(-8)	20(12)	^a / 65	^a / 61	n.a.	^a / 50
B	$(+2 - 16) / (T_{designh} - 16)$	53,85	100	36,84	2(1)	20(12)	^a / 65	^a / 49	^a / 65	^a / 41
C	$(+7 - 16) / (T_{designh} - 16)$	34,62	64,29	23,68	7(6)	20(12)	^a / 65	^a / 41	^a / 53	^a / 36
D	$(+12 - 16) / (T_{designh} - 16)$	15,38	28,57	10,53	12(11)	20(12)	^a / 65	^a / 32	^a / 39	^a / 30
E		$(TOL^e - 16) / (T_{designh} - 16)$			TOL ^e	20(12)	^a / 65	^a / ^b	^a / ^b	^a / ^b
F		$(T_{biv} - 16) / (T_{designh} - 16)$			T _{biv}	20(12)	^a / 65	^a / ^c	^a / ^c	^a / ^c
G	$(-15 - 16) / (T_{designh} - 16)$	n.a.	n.a.	81,58	-15	20(12)	^a / 65	n.a.	n.a.	^a / 57

^a At the flow rate determined at the nominal conditions in Table 15 of EN 14511-2:2018 at conditions 55/65 for fixed flow units, and at a water temperature difference of 10K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate of the unit then that minimum flow rate is used together with the outlet water temperature.

^b The variable outlet temperature is calculated by interpolation from T_{design} to the temperature closest to TOL.

^c The variable outlet temperature is calculated by interpolation from the temperatures immediately above and below T_{bivalent}.

^d If the output temperature is below the unit minimum, the unit minimum is used.

^e If TOL < T_{designh} then TOL is replaced by T_{designh}.

Test conditions for heating mode

- Water(brine)-to-water units Low temperature application

	Part load				Outdoor heat exchanger			Indoor heat exchanger			
	%				Temperatures of		Temperature	Fixed output °C	Variable output ^d		
					Input / Output		bathroom		°C		
					°C		°C				
Formula	Average	Warmer	Colder	Water	Brine	DX		Average	Warmer	Colder	
A	$(-7 - 16) / (T_{designh} - 16)$	88,46	n.a.	60,53	10 / ^b	0 / ^b	4	^a / 35	^a / 34	n.a.	^a / 30
B	$(+2 - 16) / (T_{designh} - 16)$	53,85	100	36,84	10 / ^b	0 / ^b	4	^a / 35	^a / 30	^a / 35	^a / 27
C	$(+7 - 16) / (T_{designh} - 16)$	34,62	64,29	23,68	10 / ^b	0 / ^b	4	^a / 35	^a / 27	^a / 31	^a / 25
D	$(+12 - 16) / (T_{designh} - 16)$	15,38	28,57	10,53	10 / ^b	0 / ^b	4	^a / 35	^a / 24	^a / 26	^a / 24
E	$(T_{designh} - 16) / (T_{designh} - 16)$	100			10 / ^b	0 / ^b	4	^a / 35	^a / 35	^a / 35	^a / 35
F		$(T_{biv} - 16) / (T_{designh} - 16)$			10 / ^b	0 / ^b	4	^a / 35	^a / ^c	^a / ^c	^a / ^c

^a With the flow rate determined at the standardised conditions given in Table 7 of EN 14511-2:2018 or Table 3 of EN 15879-1:2011 at conditions 30/35 for fixed flow units, and with a water temperature difference of 5K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate of the unit then that minimum flow rate is used together with the water outlet temperature.

^b With the flow rate determined at the standardised conditions given in Table 7 of EN 14511-2:2018 for fixed flow units, and with a water temperature difference of 3K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate of the unit then that minimum flow rate is used together with the inlet water temperature.

^c The variable output temperature is calculated by interpolation from the temperatures immediately above and below T_{bivalent}.

^d If the output temperature is below the unit minimum, the unit minimum is used.

Test conditions for heating mode

- Water(brine)-to-water units Intermediate temperature application

	Part load				Outdoor heat exchanger			Indoor heat exchanger			
	%				Temperatures of		Temperature	Fixed output °C	Variable output ^d		
					Input / Output		bathroom		°C		
	°C				°C		°C	°C			
Formula	Medium	Tempering	Cold	Water	Brine	DX		Medium	Tempering	Cold	
A	$(-7 - 16) / (T_{designh} - 16)$	88,46	n.a.	60,53	10 / ^b	0 / ^b	4	^a / 45	^a / 43	n.a.	^a / 38
B	$(+2 - 16) / (T_{designh} - 16)$	53,85	100	36,84	10 / ^b	0 / ^b	4	^a / 45	^a / 37	^a / 45	^a / 33
C	$(+7 - 16) / (T_{designh} - 16)$	34,62	64,29	23,68	10 / ^b	0 / ^b	4	^a / 45	^a / 33	^a / 39	^a / 30
D	$(+12 - 16) / (T_{designh} - 16)$	15,38	28,57	10,53	10 / ^b	0 / ^b	4	^a / 45	^a / 28	^a / 31	^a / 26
E	$(T_{designh} - 16) / (T_{designh} - 16)$	100			10 / ^b	0 / ^b	4	^a / 45	^a / 45	^a / 45	^a / 45
F	$(T_{biv} - 16) / (T_{designh} - 16)$				10 / ^b	0 / ^b	4	^a / 45	^a / ^c	^a / ^c	^a / ^c

^a With the flow rate determined at the standardised conditions given in Table 8 of EN 14511-2:2018 or Table 3 of EN 15879-1:2011 at conditions 40/45 for fixed flow units, and with a water temperature difference of 5K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate of the unit then that minimum flow rate is used together with the water outlet temperature.

^b With the flow rate determined at the standardised conditions given in Table 8 of EN 14511-2:2018 for fixed flow units, and with a water temperature difference of 3K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate of the unit then that minimum flow rate is used together with the inlet water temperature.

^c The variable output temperature is calculated by interpolation from the temperatures immediately above and below T_{bivalent}.

^d If the output temperature is below the unit minimum, the unit minimum is used.

Test conditions for heating mode

- Water(brine)-to-water units Medium temperature application

	Part load				Outdoor heat exchanger			Indoor heat exchanger			
	%				Inlet / Outlet temperatures		Bath temperature	Fixed output	Variable output ^d		
					°C		°C	°C	°C		
	Formula	Average	Warmer	Colder	Water	Brine	DX		Average	Warmer	Colder
A	$\frac{(-7 - 16)}{(T_{designh} - 16)}$	88,46	n.a.	60,53	10 / ^b	0 / ^b	4	^a / 55	^a / 52	n.a.	^a / 44
B	$\frac{(+2 - 16)}{(T_{designh} - 16)}$	53,85	100	36,84	10 / ^b	0 / ^b	4	^a / 55	^a / 42	^a / 55	^a / 37
C	$\frac{(+7 - 16)}{(T_{designh} - 16)}$	34,62	64,29	23,68	10 / ^b	0 / ^b	4	^a / 55	^a / 36	^a / 46	^a / 32
D	$\frac{(+12 - 16)}{(T_{designh} - 16)}$	15,38	28,57	10,53	10 / ^b	0 / ^b	4	^a / 55	^a / 30	^a / 34	^a / 28
E	$\frac{(T_{designh} - 16)}{(T_{designh} - 16)}$	100			10 / ^b	0 / ^b	4	^a / 55	^a / 55	^a / 55	^a / 55
F		$\frac{(T_{biv} - 16)}{(T_{designh} - 16)}$			10 / ^b	0 / ^b	4	^a / 55	^a / ^c	^a / ^c	^a / ^c

^a With the flow rate determined at the standardised conditions given in Table 9 of EN 14511-2:2018 or Table 3 of EN 15879-1:2011 at conditions 47/55 for fixed flow units, and with a water temperature difference of 8K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate of the unit then that minimum flow rate is used together with the water outlet temperature.

^b With the flow rate determined at the standardised conditions given in Table 9 of EN 14511-2:2018 for fixed flow units, and with a water temperature difference of 3K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate of the unit then that minimum flow rate is used together with the inlet water temperature.

^c The variable output temperature is calculated by interpolation from the temperatures immediately above and below T_{bivalent}.

^d If the output temperature is below the unit minimum, the unit minimum is used.

Test conditions for heating mode

- Water(brine)-to-water units High temperature application

	Part load				Outdoor heat exchanger			Indoor heat exchanger			
	%				Inlet / Outlet temperatures		Bath temperature	Fixed output	Variable output ^d		
					°C		°C	°C	°C		
	Formula	Average	Warmer	Colder	Water	Brine	DX	°C	Average	Warmer	Colder
A	$\frac{(-7 - 16)}{(T_{designh} - 16)}$	88,46	n.a.	60,53	10 / ^b	0 / ^b	4	^a / 65	^a / 61	n.a.	^a / 50
B	$\frac{(+2 - 16)}{(T_{designh} - 16)}$	53,85	100	36,84	10 / ^b	0 / ^b	4	^a / 65	^a / 49	^a / 65	^a / 41
C	$\frac{(+7 - 16)}{(T_{designh} - 16)}$	34,62	64,29	23,68	10 / ^b	0 / ^b	4	^a / 65	^a / 41	^a / 53	^a / 36
D	$\frac{(+12 - 16)}{(T_{designh} - 16)}$	15,38	28,57	10,53	10 / ^b	0 / ^b	4	^a / 65	^a / 32	^a / 39	^a / 30
E	$\frac{(T_{designh} - 16)}{(T_{designh} - 16)}$	100			10 / ^b	0 / ^b	4	^a / 65	^a / 65	^a / 65	^a / 65
F		$\frac{(T_{biv} - 16)}{(T_{designh} - 16)}$			10 / ^b	0 / ^b	4	^a / 65	^a / ^c	^a / ^c	^a / ^c

^a At the flow rate determined at the standardised conditions given in Table 10 of EN 14511-2:2018 or Table 3 of EN 15879-1:2011 at conditions 55/65 for fixed flow units, and at a water temperature difference of 10K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate of the unit then that minimum flow rate is used together with the water outlet temperature.

^b With the flow rate determined at the standardised conditions given in Table 10 of EN 14511-2:2018 for fixed flow units, and with a water temperature difference of 3K for variable flow units. If for any test condition the resulting flow rate is less than the minimum flow rate of the unit then that minimum flow rate is used together with the inlet water temperature.

^c The variable output temperature is calculated by interpolation from the temperatures immediately above and below T_{bivalent}.

^d If the output temperature is below the unit minimum, the unit minimum is used.